Pactitioner's Docket No. <u>U012693-7</u>

PATENT



IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

e application of: Anthony John Oliver, et al

Group No.:1621

Serial No.:09/537,250

Examiner:

Filed: March 28, 2000

For: PROCESS FOR DISTILLING FISCHER-TROPSCH DERIVED PARAFFINIC HYDROCARBONS

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Assistant Commissioner for Patents Washington, D.C. 20231

TRANSMITTAL OF CERTIFIED COPY

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Attached please find the certified copy of the foreign application from which priority is claimed for this case:

Country:

Republic of South Africa

Application

Number:

PCT/IB99/01448

Filing Date:

August 19, 1999

WARNING:

"When a document that is required by <u>statute</u> to be certified must be filed, a copy, including a photocopy or facsimile transmission of the certification is not acceptable." 37 C.F.R. 1.4(f) (emphasis added).

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CERTIFICATE OF MAILING (37 C.F.R. 1.8a)

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(Transmittal of Certified Copy-page 1 of 2) 5-4



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NOTE: "The claim to priority need be in no special form and may be made by the attorney or agent, if the foreign application is referred to in the oath or declaration, as required by § 1.63." 37 C.F.R. 1.55(a).

Sertifikagto IPE

REPUBLIEK VAN SUID-AFRIKA

Certificate

PATENTKANTOOR

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PATENT OFFICE

DEPARTEMENT VAN HAVEREN

REPUBLIC OF SOUTH AFRICA

DEPARTMENT OF TRADE AND INDUSTRY

Hiermee word gesentifiseer dat
This is to centify that the documents annexed hereto are true copies of:

Application form P.1, provisional specification and drawings of South African Patent Application No. 98/7599 as originally filed in the Republic of South Africa on 21 August 1998 in the name of SASOL TECHNOLOGY (PROPRIETARY) LIMITED for an invention entitled: "DISTILLATION";

AND it is further certified that Patent Application No. 98/7599 and the invention forming the subject matter of the patent application, together with all priority rights flowing from the patent application under the provisions of the International Convention duly were assigned accordance with law by SASOL TECHNOLOGY (PROPRIETARY) LIMITED to SCHUMANN-SASOL (SOUTH AFRICA) (PROPRIETARY) LIMITED and SULZER CHEMTECH LIMITED by virtue of Deed of concluded on 29 1999 which Assignment July Assignment was duly registered at the Patent Pretoria, on 10 August 1999;

AND it is further certified that inventor Yusuf Omar Dollie was deleted and inventor Mario Roza was added by way of an application for an amendment filed at the South African Patent Office on 11 August 1999 and allowed on 11 August 1999.

Geteken te Signed at PRETORIA in die Republiek van Suid-Afrika, hierdie 215+ dag van in the Republic of South Africa, this

Jebniary 2001

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Registrateur van Patente Registrar of Patents

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MAR 1 6 2001

REPULLIC OF SOUTH AFRIC PATENTS ACT, 1978
APPLICATION FOR A PATENT AND
ACKNOWLEDGEMENT OF RECEIPT
(Section 30(1) Regulation 22) REPUBLIC OF SOUTH AFRICA REVENUE duplicate)

060.9 **n**

21.8.98 THE GRANT OF A PATENT IS HEREBY REQUESTED BY THE UNDERMENTIONED MROMSTET ON THE BASIS OF THE PRESENT APPLICATION FILED IN DUPLICATE REPUBLIEK VAN SUID AF REPUBLIEK VAN SUID AFRIKA 387599 - CARARE HASR V123760 PATENT APPLICATION NO AANSOEKERS VERVANG APPLICANTS SUBSTITUTED 71 FULL NAME(S) OF APPLICANT(S) SASOL-TECHNOLOGY (PTY) LIMITED 1. SCHUMANIT - SASOL CSOUTH AFRICA 2 SULZER CHEMTECH ADDRESS(ES) OF APPLICANT(S) 1 STURDEE AVENUE **ROSEBANK** JOHANNESBURG, REPUBLIC OF SOUTH AFRICA TITLE OF INVENTION "DISTILLATION" Only the items marked with an "X" in the blocks below are applicable. THE APPLICANT CLAIMS PRIORITY AS SET OUT ON THE ACCOMPANYING FORM P.2. The earliest priority claimed is Country: THE APPLICATION IS FOR A PATENT OF ADDITION TO PATENT APPLICATION NO THIS APPLICATION IS A FRESH APPLICATION IN TERMS OF SECTION 37 AND BASED ON **APPLICATION NO** THIS APPLICATION IS ACCOMPANIED BY: A single copy of a provisional specification of 9 pages Drawings of 1 sheets \mathbf{x} Publication particulars and abstract (Form P.8 in duplicate) (for complete only) of the drawings (if any) for the abstract (for complete only) A copy of Figure An assignment of invention X Certified priority document(s). (State quantity) Translation of the priority document(s) An assignment of priority rights A copy of Form P.2 and the specification of RSA Patent Application No Form P.2 in duplicate X A declaration and power of attorney on Form P.3 X Request for ante-dating on Form P.4 Request for classification on Form P.9 Request for delay of acceptance on Form P.4 Extra copy of informal drawings (for complete only)

ADDRESS FOR SERVICE: Adams & Adams, Pretoria

Dated this 21 day of August 1998

ADAMS & ADAMS APPLICANTS PATENT ATTORNEYS

The duplicate will be returned to the applicant's address for service as proof of lodging but is not valid unless endorsed with official stamp

1998 -08- 21 REGISTRATEUR VAN PATENTE, MODELLE HANDELSMERKE EN OUTEURSREG REGISTRAR OF PATENTS

EGISTMAN OF PATENTS, DESIGNS, TRADE MARKIS AND CORVEIGHT

A&A P201

REPUBLIC OF SOUTH AFRICA PATENTS ACT, 1978 DECLARATION AND POWER OF ATTORNEY

			-i	(Section 30 - Regulatio	n 8, 22(i)(c) and 3	33)				
PAT	PATENT APPLICATION NO			A&A Ref: V12946 GSK			LODGING DATE			
21	01	98/7599				2:	2	21 AU	GUST 19	98
FUL	L NAN	ME(S) OF APPLICANT(S)			: 				
71		SASOL TECHNOLOGY	' (PRC	OPRIETARY) LIMI	TED					
FUL	L NAN	ME(S) OF INVENTOR(S	5)	ĺ						
72		1. OLIVIER, Anthony 3. DUCKITT, Charles 5. ADAMS, Vernon Je 7. CALDER, Roy Alex	erema	4. RA y 6. M	CHTER, Ferd AMDUTH, A OODLEY, Vid OZA, Mario	shwin				
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54		"DISTILLATION"				1 .		-11- 22		
**	I/We here	VAN DER MERW by declare that :- - I/we am/are the application	*	× -		REGISTRAT HANDEL	EUR VA SMERI	IN PATENTE, I (E EN OUTEU	MODELLE, RSREG	٠.
**	2.	I/we have been authori stated in the capacity o	zed by		make this dec	claration an	d have	e knowledge	of the fa	icts hereii plicant(s)
***	3.	the inventor(s) of the all acquired the right to ap	bovem ply by	entioned invention virtue of an assign	is/are the personment from th	on(s) name e inventor(d abov s);	ve and the a	pplicant(s) has/hav
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In the case of application in the name of a company, partnership or firm, give full names of signatory/signatories, delete paragraph 1, and enter capacity of each signatory in paragraph 2.

If the applicant is a natural person, delete paragraph 2.

If the right to apply is not by virtue of an assignment from the inventor(s), delete 'an assignment from the inventor(s)' and give details of acquisition of right. For non-convention applications, delete paragraph 5.

ADAMS & ADAMS PATENT ATTORNEYS **PRETORIA**

FORM P6

REPUBLIC OF SOUTH AFRICA Patents Act, 1978

PROVISIONAL SPECIFICATION

(Section 30 (1) - Regulation 27)

LODGING DATE 21 OFFICIAL APPLICATION NO

98/7599

21 AUGUST 1998

71 FULL NAME(S) OF APPLICANT(S) • AANSOEKERS VERVANG

SASOL TECHNOLOGY (PROPRIETARY) LIMITED 1. SCHÜMANN-SAFOL (SONTH AFRICA) (PTY) LTD 2. SULZER CHEMTECH LTD

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8. MARIO ROZA

TITLE OF INVENTION

"DISTILLATION"

THIS INVENTION relates to distillation. More particularly, the invention relates to a process for distilling paraffinic hydrocarbons, particularly Fischer-Tropsch derived paraffinic hydrocarbons.

5 According to the invention, there is provided a process for distilling paraffinic hydrocarbons, which process comprises

feeding a Fischer-Tropsch derived paraffinic hydrocarbon feedstock comprising. heavy paraffinic hydrocarbons and, optionally, light and/or medium paraffinic hydrocarbons, into a 10 distillation column;

operating the distillation column to produce usable wax products; and

withdrawing from the distillation column an overhead stream, a bottom stream, and at least one side stream, with the bottom stream and/or the side stream comprising usable wax products.

By 'usable' in respect of the wax products is meant that the wax products are non-thermally degraded. These products will normally also meet stringent specifications with respect to properties such as congealing point, methyl-ethyl-ketone solubles, penetration, differential scanning calorimetry curves etc.

By 'Fischer-Tropsch derived' is meant paraffinic products obtained by subjecting a synthetic gas comprising carbon monoxide (CO) and hydrogen (H₂) to Fischer-Tropsch reaction conditions in the presence of an iron-based, a cobalt-based or an iron/cobalt-25 based Fischer-Tropsch catalyst. The products of the Fischer-Tropsch reaction are predominantly n-paraffinic, although some isomers, olefins, oxygenates and other functional groups may also be produced. The products from the Fischer-Tropsch reaction have a wide boiling range. Prior to using the products from the 30 Fischer-Tropsch reaction as a feedstock for the present process,

they may optionally be hydrogenated. Such hydrogenation may be effected by contacting the Fischer-Tropsch reaction products with hydrogen in the presence of a hydrogenation catalyst, at elevated temperature and pressure, in known fashion.

- 5 The Fischer-Tropsch reaction conditions include using a relatively low reaction temperature in the range 180-300°C, typically 210-260°C, so that a so-called low temperature Fischer-Tropsch synthesis is employed, and the Fischer-Tropsch reaction is typically effected in a fixed or slurry bed reactor.
- 10 The feedstock may comprise, in addition to the heavy paraffinic hydrocarbons, the light and the medium paraffinic hydrocarbons. The feedstock could thus typically have a true boiling point curve as indicated in Table 1:

TABLE 1: True boiling point (TBP) curve of a typical Fischer-15 Tropsch derived feedstock .

	Mass %	TBP (°C)
20	1 5 10 30 50 70 90	142 169 195 313 417 550 716
25	95 98	757 831

The feedstock typically comprises hydrocarbon molecules in the range C_{3+} to C_{220+} . Products with carbon ranges of C_{20-} , C_{10} to C_{40} and C_{15} to C_{220} or higher, are deemed light, medium and heavy hydrocarbons respectively.

30 The distillation column can be operated to produce paraffins (C_{23-}) , medium wax $(C_{20}$ to $C_{38})$, and hard wax (C_{30+}) or combinations thereof, with these products then being withdrawn in the overhead stream, the bottom stream or in the at least one side stream. All the wax products produced will thus be usable wax products as hereinbefore defined.

Preferably, however, a plurality of side streams are withdrawn from the column, with each side stream comprising a component of the paraffins, a component of the medium wax, or a component of the hard wax, or combinations thereof.

- 5 The distillation column is preferably operated under vacuum. Thus, the pressure in the column may be in the range of 1 to 12 mbar(a), typically 8 to 10 mbar(a). The temperature in the column sump may then be in the range of 190°C to 340°C, typically in the range of 295°C to 300°C.
- 10 It is preferred to operate the column under vacuum, to prevent, or at least inhibit, thermal degradation of the feedstock and the products. Such thermal degradation will have a negative effect on the properties of the products produced, such as on the congealing point, penetration and oil content of the wax 15 products.

The process may include feeding stripping steam into the distillation column, to adjust the relative volatility of components in the feedstock. The process may also include feeding one or more of the side streams through a stripping stage. It is envisaged that steam stripping can be used to adjust the front end volatility of the products, thereby to aid in product quality.

The distillation column may comprise structured packing typically having a surface area (in m²) to volume (in m³) ratio of 125:1 25 to 750:1, e.g. 250:1, 350:1 or 500:1, or any other intermediate value.

This packing and internal arrangement of the distillation column produces a very low pressure drop and minimal entrainment, while ensuring that the required separation is achieved. Typically, 30 five theoretical stages are provided, with the respective stages each containing the packing and the internal arrangement and each stage being located between draw points for the overhead, side and bottom streams from the column. The packings of the various stages can have the same surface area to volume ratios, or the

surface area to volume ratios of the packings of at least some of the stages can be different. The internal arrangement minimizes the residence time within the distillation column, thus reducing the amount of thermal cracking of the products produced.

5 The process of the invention thus employs multiple side streams with separation stages in the column between the withdrawal of the side streams, to split wax fractions.

With the process of the invention, the Fischer-Tropsch derived feedstock is thus fractionated into product streams having unique 10 properties. One of these properties is the congealing point, which can thus be used to control the operation of However, instead, or additionally, other distillation column. unique properties, such as methyl-ethyl-ketone (MEK) / methylisobutyl-ketone (MIBK) solubles, penetration at 25°C, carbon etc. can be used to control distillation 15 distributions, The number of side streams from the column are determined by the properties of the products and by product purity desired. There is, in principle, no restriction on the maximum number of side stream product draws other than the fact 20 that the accumulated pressure drop of the internals must be limited.

The invention will now be described by way of example, with reference to the accompanying drawing and non-limiting example.

In the drawing, reference numeral 10 generally indicates, in 25 simplified flow diagram form, a process according to the invention for distilling paraffinic hydrocarbons.

In the drawing, reference numeral 10 generally indicates a process according to the invention, for distilling a Fischer-Tropsch derived light, medium and heavy paraffinic hydrocarbon 30 feedstock.

The process 10 includes a distillation column 12 having six vertically staggered packing stages 14, 16, 18, 20, 22 and 24. Each packing stage comprises high performance structured packing

and associated internals such as structured packing having a surface area (in m^2) to volume (in m^3) ratio of 125:1, 250:1, 350:1, 500:1 or 750:1, or any appropriate intermediate value..

A feed line 26 leads into the bottom of the distillation column 5 12, as does a stripping steam feed line 28. Into the line 26 leads a light (C_{20}) hydrocarbon line 30, a medium $(C_{10} - C_{40})$ hydrocarbon line 32 and a heavy $(C_{15} - C_{220})$ hydrocarbon line 34.

The feed line 26 and the stripping steam feed line 28 lead into the column below the lowermost packing stage 14.

10 A bottoms line 36 leads from the bottom of the column 12.

A side stream line 38 leads from the column between the packing stages 14, 16 to a stripping column 40, with a stripping steam line 42 leading into the bottom of the column 40. The column 40 comprises a packing stage 44 comprising sieve trays. A product line 46 leads from the bottom of the column 40, while a return line 48 leads from the top of the column 40. The return line 48 returns to the column 12 between the packing stages 16, 18.

A side stream withdrawal line 50 leads from the distillation column between the packing stages 16, 18 into a stripping column 20 52 having a packing stage 54 comprising sieve trays. A product withdrawal line 56 lead from the bottom of the column 52, while a return line 58 leads from the top of the column 52 back to the distillation column 12 between the packing stages 18, 20.

A side stream withdrawal line 60 leads from the column 12 between 25 the packing stages 18, 20. The line 60 leads into the top of a stripping column 62 having a packing stage 64 comprising sieve trays. A product withdrawal line 66 leads from the bottom of the column 62, while a return line 68 leads from the top of the column 62 back to the distillation column 12 between the packing 30 stages 20, 22.

A side stream withdrawal line 70 leads from the distillation column 12 between the packing stages 20, 22. The line 70 leads

into a stripping column 72 having a packing stage 74 comprising sieve trays. A product withdrawal line 76 leads from the bottom of the column 72, while a return line 78 leads from the top of the column 72 back to the distillation column 12, between the 5 packing stages 22, 24.

A side stream/product withdrawal line 80 leads from the distillation column 12 between the packing stages 22, 24, and is fitted with a recycle line 82 returning to the distillation column 12 above the packing stage 24.

10 An overheads line 84 leads from the top of the column.

In use, a Fischer-Tropsch derived light, medium and heavy hydrocarbon feedstock is fed, along the flow line 26, into the bottom of the distillation column 12. The distillation column 12 is typically operated at a pressure of 8-10 mbar(a) and at a temperature, measured in the column sump, of about 295-300°C.

Usable wax products, such as medium wax $(C_{20} - C_{38})$ and hard wax (C_{30+}) are produced in the column 12.

The products withdrawn along the lines 36, 46, 56, 66, 76, 80 and 84 typically comprise C_{35+} , C_{25} - C_{40} , C_{20} - C_{30} , C_{19} - C_{23} , C_{18} - 20 C_{20} , C_{17-} and C_{5-} respectively.

Stripping steam lines 86 lead into the bottoms of each of these stripping columns 52, 62, 72.

The following non-limiting example was also conducted, in a simulation of the process 10:

25 EXAMPLE

The feedstock entering the column 12 along the line 26 comprised light hydrocarbons (also known and referred to as Cold Condensate (CC)), medium hydrocarbons (also known and referred to as Hot Condensate (HC)) and heavy hydrocarbons (also known and referred to as Reactor Waxes (RW)). All the hydrocarbons were Fischer-

Tropsch derived. Thus, each component of the feedstock was a blend of the respective products from both fixed and slurry bed reactor Fischer-Tropsch processes. The blend ratio in this example was:

CC = 28.8 % by mass

HC = 17.2 %

RW = 54.0 %

The above blend ratio was dictated by the production rates from the existing fixed and slurry bed Fischer-Tropsch reactor processes. Blend ratios of only slurry bed or fixed bed products can be used as well.

The number of side streams from the column 12 are determined by the properties of the product or the by-product purity desired.

There is no restriction on the maximum number of side product streams other than the fact that the accumulated pressure drop of the internals must be limited. If unlimited, energy loss and thermal cracking can be so significant that the process becomes technologically and/or economically non-viable.

Table 2 hereunder shows the streams produced, the desired 20 congealing point (CP) range and typical CP values obtained.

:		Product	Name	CP Desired Range (°C)	Typical CP obtained (°C)
	Overhead Stream 84	C ₅ -	Gas	n/a	n/a
	Stream 80	C ₁₇₋	C ₁₇ -Paraffins	n/a	n/a
	Stream 76	C ₁₈ -C ₂₀	C ₁₈ -C ₂₀ Paraffins	25-30	28
25	Stream 66	C ₁₉ -C ₂₃	Waksol	35-40	38
	Stream 56	C ₂₀ -C ₃₀	Medium Wax 1	50-55	53
	Stream 46	C ₂₅ -C ₄₀	Medium Wax 2	60-65	64
	Bottom Stream 36	C ₃₅₊	Hard Wax	65+	98

The yield of the above streams on a mass basis as a percentage of the feed was approximately:

. •	Overhead Stream 84			= .	1.0	ે
	Stream	80	:	=	27.6	8
5	Stream	76	:	=	5.8	⁸
	Stream	66	;	=	4.5	[%]
	Stream	56	;	=	6.9	8
	Stream	46	•	=	11.4	ફ
	Bottom	Stream	36	=	42.8	ે

10 The column 12 was operated at 9 mbar(a) using a four stage steam ejector for its vacuum system. It had six packed beds with low pressure drop structured packing, each bed comprising of Sulzer 250Y (trade mark) packing available from Sulzer Chemtech Ltd, PO Box 65, CH-8404, Winterthur, Switzerland. Some side streams had side stripper columns as indicated in the drawing. Low pressure (2.4 bar_g) steam was injected into both the bottom of the main fractionator and the side stripper columns to aid in separation.

The process 10 permits a light, medium and heavy Fischer-Tropsch derived feedstock to be distilled into normal usable product 20 ranges using a single column with multiple product side streams. This has hitherto not been possible due to high pressure drops associated with conventional pattern of distillation columns. The wax products produced are usable wax products.

The process 10 is capable of producing a wide range of narrow 25 cuts, and also has substantial flexibility.

DATED THIS 21ST DAY OF AUGUST 1998

ADAMS & ADAMS APPLICANT'S PATENT ATTORNEY